

Remarks

The final Office Action dated May 13, 2009 has been carefully considered. Applicants have amended claims 27 and 38 without the addition of new matter. Applicants have cancelled claim 36 without prejudice to the subject matter therein. Applicants have added new claims 56, 57, and 58 without the addition of new matter.

Statement Of The Substance Of The Interview

Attorney for Applicants thanks Examiner Kugel for the courtesies extended during the telephonic interview conducted on 29 July 2009. Attorney for Applicants generally agrees with the Interview Summary dated 3 August 2009, prepared by Examiner Kugel in connection with that telephonic interview.

As discussed during that interview, Applicants include with this response a certified translation of the priority document DE 102 43 312.7 filed 18 September 2002, attached hereto as Appendix A. Applicants have now perfected the claim to priority under MPEP § 706.02(b). Applicants respectfully request reconsideration of the current claims in view of the perfected priority and the following remarks.

Claim Rejections – 35 USC § 102 and/or 103

In Paragraph 6 of the Office Action, claims 27-30, 32-36, 38 and 41-38 are rejected under 35 USC 102(e) as being anticipated by or, in the alternative, under 35 USC 103(a) as being unpatentable over Kirsner. Applicants assume the examiner meant to reject claims 27-30, 32-36, 38, and 41-48 and are responding as such. Applicants submit the rejection is in error as Kirsner is not prior art under 102(e) nor under 103(a).

Kirsner has been cited as a 102(e) prior art. Section 102(e) states that

A person shall be entitled to a patent unless . . . (e) the invention was described in (1) an application for patent, published under section 122(b), by another filed in the United States before the invention by the applicant for patent or (2) a patent granted on an application for patent by another filed in the United States before the invention by the applicant for patent, except that an international application filed under the treaty defined in section 351(a) shall have the effects for the purposes of this subsection of an application filed in the United States only if the international application designated the United States and was published under Article 21(2) of such treaty in the English language. . . .

Kirsner was filed November 12, 2002 and published July 31, 2003 (2003/0144153).

Kirsner is a continuation-in-part of U.S. Application No. 10/175,272, filed on June 19, 2002, which is a continuation-in-part of U.S. Application No. 09/929,465, filed August 14, 2001 and International Patent Application Nos. PCT/US00/35609 and PCT/US00/35610, both filed December 29, 2000. The new matter found in Kirsner (2003/0144153) relates to the toxicity levels of the composition disclosed therein. *See ¶¶ [0100]–[0102]*. The prior Kirsner applications do not disclose the toxicity element of the present application. As such, Kirsner (2003/0144153) is not a prior art reference under section 102(e) or 103(a) because it was not filed, nor can it claim a priority date in relation to the toxicity levels, prior to the current applications' earliest priority date of September 18, 2002 (DE 102 43 312.7). Applicants respectfully submit the 102(e) and 103(a) rejections were in error and request the examiner withdraw the rejection of claims 27-30, 32-36, 38, and 41-48.

In light of the above-arguments and amendments to the claims, Applicants submit the rejection is in error and request the examiner reconsider the claims 27-30, 32-36, 38 and 41-48.

In Paragraph 7 of the Office Action, claims 39 and 40 are rejected under 35 USC § 103(a) as being unpatentable over Kirsner as applied to claims 27-30, 32-36, 38 and 41-38 above in view of Muller '954. As discussed above, Kirsner does not qualify as prior art. Applicants therefore respectfully request the examiner withdraw the rejection of claims 27-30, 32-36, 38 and 41-48.

Conclusion

In view of the amendments and remarks presented herein, Applicants submit that the present application is in condition for allowance, and such action is respectfully requested. If, however, any issues remain unresolved, the Examiner is invited to telephone Applicants' counsel at the number provided below.

Respectfully submitted,

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APPENDIX A

OC84123PCUS

VERIFICATION OF TRANSLATION

I, Dr. Martin Herzog - patent attorney

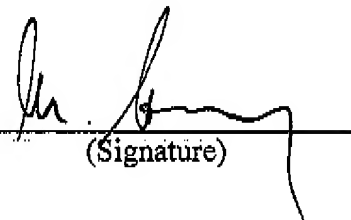
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declare as follows:

1. That I am well acquainted with both the English and German languages, and
2. that the attached document is a true and correct English translation controlled by me to the best of my knowledge and belief of:
 - German priority application 102 43 312.7

August 06, 2009

(Date)



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Borehole treatment compositions with low-toxicity oil phase

The invention relates to borehole treatment compositions which comprise an aqueous phase and an oil phase, this oil phase exhibiting particularly low levels of toxicity towards marine microbiota.

Borehole treatment compositions encompass all kinds of auxiliary fluids which can be used when drilling into reserves of petroleum or natural gas. As a characteristic example of such treatment compositions, the invention is described below with reference to drilling fluids and drilling muds based thereon which may be used both with land-sited and with marine wells. The field of use of the inventive modification of auxiliary fluids of the type concerned here, however, is not restricted to these systems. It also embraces the numerous further auxiliary fluids of the field which is addressed here. Examples that may be mentioned include spotting fluids, spacers, packer fluids, auxiliary fluids for workover and stimulation and for fracturing. The invention is directed both to auxiliary fluids of the type stated which are oil-based, i.e. operate with a continuous oil phase, and to auxiliaries in which the oil phase is emulsified in a continuous phase which in particular is aqueous. Drilling fluids and drilling muds based on them are characteristic examples of the various possibilities.

On the one hand, are known water-based drilling muds which have an emulsified oil phase content of approximately 1 to 50%, in addition to the other customary auxiliaries of such a drilling mud, which are also referred to as O/W emulsion muds. On the other hand, oil-based mud systems in which the oil constitutes the flowable phase or else at least a substantial fraction of the flowable phase in the form of a continuous oil phase are in widespread use. Particular importance here attaches to the muds known as invert drilling muds, which on the basis of W/O emulsions comprise a disperse aqueous phase in the continuous oil phase. The amount of disperse aqueous phase is normally in the range from at least about 5 to

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10% by weight up to about 50 to 60% by weight. In addition to these W/O invert drilling muds, those referred to as true oil muds are also known, whose liquid phase is composed almost exclusively of a continuous oil phase and which contain small amounts if any – normally not more than about 5 to 10% by weight – of aqueous phase in dispersed form.

The non-aqueous phase of such mud systems is formed by what is called the carrier fluid. This is generally diesel oil, to which certain additives are added to form the actual drilling mud. With the end of the 1980s, however, came the demand for environment-friendly mud systems and hence carrier fluids. These were in particular to be more biodegradable than the diesel oil used beforehand. Alongside various liquid esters, such as those described in EP 0 374 672 A1, for example, olefinic hydrocarbons were investigated for their usefulness. Reference may be made here, by way of example, to the applicant's EP 0 765 368 A1, which is directed to the use of alpha-olefins as carrier fluids.

There nevertheless continues to be a need for novel carrier fluids, since the known compounds frequently cannot be used under all operating conditions or do not meet the increasingly stringent requirements for biodegradability or low toxicity. The latter criterion in particular is becoming increasingly significant, since more and more wells are destined to be sunk in ecologically sensitive regions. This is especially the case with offshore wells, i.e. wells sunk in the ocean floor.

The toxicity of a mud is generally determined by biological tests in which marine microbiota are exposed to the ingredients of the mud at different concentrations. The objective is to find mud systems which meet the physical, technical requirements while being of minimal toxicity to the environment. Mention should also be made at this point of the physical stresses on the drilling muds. The muds are heated at great depths to high temperatures, up to 250°C or more; high pressures prevail, and at the same time the compounds in the mud both must remain chemically stable and must not exhibit any severe change in their viscosity behaviour, while continuing to form a stable emulsion under the conditions outlined.

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It is an object of the present invention to provide borehole treatment compositions, especially drilling muds, which are enhanced both in respect of their performance properties and in respect of environmental compatibility.

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The present specification accordingly provides borehole treatment compositions comprising an aqueous phase and a non-aqueous oil phase, emulsifiers and, where appropriate, further customary additives, such as weighting agents, fluid loss additives, viscosity regulators, wetting agents, salts, biocides, corrosion inhibitors
10 and/or an alkali reserve, the non-aqueous phase being selected in whole or in part from the group consisting of

- a) paraffins having from 5 to 22 carbon atoms and/or
- b) internal olefins having from 12 to 30 carbon atoms in the molecule
in each case in the form of a blend with
- 15 c) carboxylic esters of the general formula $R-COO-R'$, where R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical having from 3 to 22 carbon atoms

20 or from mixtures of components a) to c), characterized in that the ratio of the toxicity of internal olefins of chain length C16/C18 (standard IO) to the toxicity of the constituents of the non-aqueous phase, in each case measured by the *Leptocheirus plumulosus* acute, static 96 hour/10 day sediment toxicity test (in accordance with ASTM E 1367 – 92 & EPA/600/R-94/025, Section 11), is less than 1.

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Toxicity testing by means of the abovementioned *Leptocheirus* test in accordance with ASTM E 1367 is prescribed by the Environmental Protection Agency (EPA) for drilling fluid systems intended for use in wells in the Gulf of Mexico. In order to make it easier to compare results, the toxicity for a standard compound, namely

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a mixture of internal olefins of chain lengths C16/C18, is compared with the results for the carrier fluids to be tested. The ratio F (relative toxicity) is determined as follows: $F = \text{toxicity (standard)}/\text{toxicity (carrier fluid)}$. The muds of the invention comprise oil phases for which the value of F is less than 1, preferably less than 0.5, and in particular cases less than 0.4.

As the toxicity investigations demonstrate, hydrocarbons are extremely critical in respect of the *Leptocheirus plumulosus* results. The table below illustrates this:

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Hydrocarbon compounds used as carrier fluids	F
Branched paraffins	2.7 – 4.53
LAO C14/16 70:30	3.15
Low-tox. mineral oil	17.41
C16/18 IO	1.19 – 1.94

- The results which show that esters – based on C16-C26 total carbon chains – are able to bring the overall toxicity of mixtures of hydrocarbons with ester into line with the criteria set by the EPA are all the more surprising. Listed below are exemplary mixtures, together with their F values:

Oil phase		Mixing ratio	F
Branched paraffin			= 2.7
Branched paraffin	+ C20-22 = (OMC 586)	70:30	=0.98/0.54
Branched paraffin	+ C20-22 = (OMC 586)	60:40	= 0.36
Branched paraffin	+ C20-22 = (OMC 586)	50:50	= 0.37
Branched paraffin	+ C21 = (OMC 233)	50:50	= 0.37
C16/C18 IO			= 2.7
C16/18 IO + C16-18 (OMC 1049)		50:50	= 0.87
C16/18 IO + mix of C16-C18+C20-22		40:40:20	= 0.90

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C16/C18 IO +C16-C26 blend		50:50	= 0.96
LAO C14/16 70:30	+ C20-22 OMC 586	50:50	= 2.5
Low-tox. mineral oil	+ C20-22 OMC 586	50:50	= 2.3

OMC586 denotes a 2-ethylhexanol ester based on saturated C8-C14 fatty acids. OMC233 corresponds to an isobutanol ester based on C14-18 + C16-18 unsaturated fatty acids. OMC1049 denotes 2-ethylhexyl octanoate. All of the products are
5 from Cognis.

The results show that of the products already used in drilling practice, such as branched paraffins, LAO 14/16, low-tox. mineral oil and IO C16/18, the two products C14/16 LAO and the low-tox. mineral oil (as a result of no acceptable addition
10 of ester) can be brought into line with the data for the EPA reference substance (IO C16/18 from Chevron). This is particularly surprising in respect of LAO, since branched paraffins generally have the greater toxicity. The data show, however, that it is possible, by adding esters or ester mixtures in accordance with the invention, to prepare drilling mud systems based on IO and also liquid paraffins
15 (branched and linear) which achieve a *Leptocheirus* toxicity factor <1.

The oil phases of the systems of the invention comprise components a) and/or b) alone or together in a blend with esters c) and also, where appropriate, in a blend with other suitable oil phases.

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Component a)

As component a), use is made in accordance with the invention of linear or branched paraffins having from 5 to 22 carbon atoms. Paraffins – more correctly

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referred to alkanes – are, as is known, saturated hydrocarbons, which for the linear and branched representatives follow the general empirical formula C_nH_{2n+1} . The cyclic alkanes follow the general empirical formula C_nH_{2n} . Particular preference is given to the linear and branched paraffins, whereas cyclic paraffins are less preferred. The use of branched paraffins is particularly preferred. Also preferred are paraffins which are liquid at room temperature, in other words those having from 5 to 16 carbon atoms per molecule. However, it may also be preferred to use paraffins of 17 to 22 carbon atoms which have a waxlike consistency. It is preferred, however, to use mixtures of the different paraffins, and particularly preferred if these mixtures are still liquid at 21°C. Such mixtures may be formed, for example, from paraffins having from 10 to 21 carbon atoms. As far as the toxicity is concerned, especially in the *Leptocheirus plumulosus* test, the performance of paraffins alone is generally inadequate. Typical F values for paraffins lie between 2.7 and 4.53.

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Component b)

As component b) it is possible in accordance with the invention to use internal olefins (abbreviated below to IO). IOs are likewise compounds known per se which can be prepared by any of the processes that are known to the person skilled in the art for that purpose. EP 0 787 706 A1, for example, describes a process for synthesising IOs by isomerising alpha-olefins over sulfonic or persulfonic acids. A characteristic feature is that the IOs thus obtained are linear and contain at least one olefinic double bond which is not in the alpha position in the alkyl chain.

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In accordance with the invention it is preferred to use those IOs and IO mixtures which comprise IOs having from 12 to 30 carbon atoms per molecule, preferably having 14 to 24 carbon atoms and in particular having up to 20 carbon atoms per molecule. The olefins used in accordance with the invention preferably contain

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only one olefinic double bond. In the Leptocheirus test, F values of between 1.1 and 2.0 are typically achieved.

Component c)

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A further constituent of the oil phases of the invention are esters of the general formula $R-COO-R'$, in which R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical having from 6 to 22 carbon atoms. Esters of
10 this kind are also known chemical compounds. Their use in principle in drilling muds is the subject-matter, for example, of EP-0 374 672 A1 and of EP 0 374 671 A1. The Leptocheirus values for esters are typically in the range from 1.5 to 0.2, so that such compounds alone may already be suitable for forming oil phases of low toxicity. However, particular chain lengths must be selected to
15 that end. Particular preference is given to using esters whose radical R stands for a saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and whose radical R' stands for a saturated alkyl radical having from 3 to 10 carbon atoms. In particular, the saturated compounds here are preferred. In the context of the inventive teaching it is preferred for the oil phase to contain, besides the esters
20 as described above, not more than 15% by weight (based on the oil phase) of other esters having radicals R which stand for alkyl radicals having more than 23 carbon atoms.

The present invention therefore further provides drilling muds which, in addition to
25 the aqueous phase, comprise as oil phase only those esters of the above general formula whose toxicity, measured by the Leptocheirus test, is less than 1 in comparison to the standard IO. The present specification therefore also claims drilling muds comprising an aqueous phase and a non-aqueous oil phase, emulsifiers and, where appropriate, further customary additives, such as weighting agents, fluid loss
30 additives, viscosity regulators, wetting agents, salts, biocides, corrosion inhibitors

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and/or an alkali reserve, more than 50% by weight of the non-aqueous phase being selected from the group consisting of esters of the general formula $R-COO-R'$ where R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical having from 3 to 10 carbon atoms, the non-aqueous phase having a relative toxicity, i.e. the ratio of the toxicity of internal olefins of chain length C16/C18 (standard IO) to the toxicity of the constituents of the non-aqueous phase, measured in each case in accordance with the *Leptocheirus plumulosus* acute, static 96 hour/10 day sediment toxicity test (in accordance with ASTM E 1367 – 92 & EPA/600/R-94/025, Section 11), of less than 1.

Besides components a) and/or b) and c) it is possible for the oil phases to include other, water-insoluble constituents, provided that they are environmentally compatible. Specific further particularly suitable mixture components of the oil phases of the invention are therefore:

(i) esters of C1-5 monocarboxylic acids and mono- and/or polyfunctional alcohols, the radicals of monohydric alcohols having at least 6, preferably at least 8, carbon atoms and the polyhydric alcohols possessing from 2 to 6 carbon atoms per molecule,

(ii) mixtures of secondary esters selected from the group consisting of propyl carboxylate, butyl carboxylate, pentyl carboxylate, hexyl carboxylate, heptyl carboxylate, octyl carboxylate, nonyl carboxylate, decyl carboxylate, undecyl carboxylate, dodecyl carboxylate, tridecyl carboxylate, tetradecyl carboxylate, pentadecyl carboxylate, hexadecyl carboxylate, heptadecyl carboxylate, octadecyl carboxylate, nonadecyl carboxylate, eicosyl carboxylate, uneicosyl carboxylate, docicosyl carboxylate and isomers thereof, the secondary esters each having a carboxylate radical of 1 to 5

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carbon atoms, water-insoluble ethers of monohydric alcohols having from 6 to 24 carbon atoms,

(iii) water-insoluble alcohols having from 8 to 36 carbon atoms,

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(iv) poly-alpha-olefins (PAO) and alpha-olefins

(v) mixtures of components (i) to (v).

10 Excluded from use, however, are linear alpha-olefins of chain lengths C14/C16 and also what are termed *low toxicity* mineral oils, since these do not achieve the desired toxicity levels even when blended, in accordance with the invention, with esters from group c). Likewise excluded is the use of diesel oil. Also excluded, moreover, is the use of methyl esters, since their high toxicity makes them unsuit-
15 able for constituting low-toxicity oil phases in the sense of the invention. Under certain conditions, however, the use of such constituents may be necessary – in that case, however, the amounts used are not more than 5% by weight, preferably not more than 2% by weight, based on the oil phase.

20 As a further mandatory constituent, the compositions of the invention comprise emulsifiers. Their selection depends critically on the type of mud. Emulsifiers which can be used in practice for forming W/O emulsions are, in particular, selected oleophilic fatty acid salts, examples being those based on amido amine compounds. Examples thereof are described in the above-cited US-A 4,374,737
25 and the literature cited therein.

For preparing W/O emulsions, however, other, preferably nonionic, emulsifiers are used. From the wide range of nonionic emulsifiers, emulsifiers which are particularly suitable in accordance with the invention can be assigned to at least one of the following classes of substance: (oligo)alkoxylates – especially lower alkoxylates,

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with corresponding ethoxylates and/or propoxylates being of particular significance here – of parent molecules of natural and/or synthetic origin which contain lipophilic radicals and are amenable to alkoxylation. "Lower" in this context denotes from 2 to 15, and in particular from 2 to 10, parts of alkoxide per molecule of
5 emulsifier. Another important class of nonionic emulsifiers for the purposes of the invention are partial esters and/or partial ethers of polyfunctional alcohols having in particular from 2 to 6 carbon atoms and from 2 to 6 OH groups and/or their oligomers with alcohols and/or acids containing lipophilic radicals. Also suitable in particular in this context are compounds of this kind which additionally contain
10 (oligo)alkoxy radicals and, in particular, corresponding oligoethoxy radicals incorporated into their molecular structure. A further example of corresponding emulsifier components are alkyl (poly)glycosides of long-chain alcohols and also the aforementioned fatty alcohols of natural and/or synthetic origin, and alkylolamides, amine oxides and lecithins. With no claim to completeness, mention may be made
15 additionally, from the classes of suitable emulsifiers components cited here, of the following representatives: the (oligo)alkoxylates of parent molecules containing lipophilic radicals may derive in particular from selected representatives of the following classes of parent molecules containing lipophilic radicals: fatty alcohols, fatty acids, fatty amines, fatty amides, fatty acid and/or fatty alcohol esters and/or
20 ethers, alkanolamides, alkylphenols and/or reaction products thereof with formaldehyde, and also further reaction products of carrier molecules containing lipophilic radicals with lower alkoxides. Particular examples of partial esters and/or partial ethers of polyfunctional alcohols are the corresponding partial esters with fatty acids, for example of the type of the glycerol monoesters and/or diesters, glycol monoesters, corresponding partial esters of oligomerised polyfunctional alcohols, sorbitan partial esters and the like, and also corresponding compounds with
25 ether groups.

The oil phases are preferably formed by mixtures of components a) and/or b) with
30 the ester oils c) in a weight ratio of from 10:1 to 1:1, preferably from 5:1 to 1:1 and in particular from 3:1 to 1:1, in order to achieve the desired relative toxicity.

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The borehole treatment compositions of the present invention are preferably in the form of a water-in-oil (W/O) emulsion, i.e., a homogeneous oil phase encloses the finely disperse aqueous phase. With particular preference, the present compositions of the invention are configured as drilling muds. The compositions of the invention preferably have a weight ratio between the aqueous phase and the oil phase of from 50:50 to 1:99, preferably from 30:70 to 20:80 and in particular 10:90. It is preferred for at least 50% by weight, preferably at least 80% by weight and in particular at least 90% by weight of the oil phase to be composed of compounds a) and/or b) and c). Preference is further given to borehole treatment compositions in which at least 50% by weight, preferably at least 80% by weight and in particular 100% by weight of the oil phase is formed by components a) to c). The percentages by weight here are based on the weight of the oil phase.

It may be advantageous for 100% by weight of the non-aqueous oil phase of the compositions of the invention to be composed of blends of component a) and/or b) and c). It may further be advantageous if only mixtures of a) and c) or, preferably, only b) and c) are present in the oil phases of the compositions of the invention.

The oil phases of the compositions of the invention preferably have pour points of below 0°C, preferably of below -5°C, measured in accordance with DIN ISO 3016: 1982-10). The Brookfield viscosity of the oil phases at 0°C is not more than 50 mPas. Where they are in the form of an oil-based drilling mud of the W/O type, the borehole treatment compositions of the invention have a plastic viscosity (PV) in the range from 10 to 70 mPas and a yield point (YP) of from 5 to 60 lb/100 ft², measured in each case at 50°C. The kinematic viscosity of the oil phase, measured by the Ubbelohde method at 20°C, ought preferably to be not more than 12 mm²/s. The aqueous phase of the compositions of the invention preferably has a pH in the range from 7.5 to 12, more preferably from 7.5 to 11 and in particular from 8 to 10.

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Besides the constituents set out above, the compositions of the invention further comprise additives, examples being weighting agents, fluid loss additives, viscosity regulators, wetting agents, salts, biocides, corrosion inhibitors and/or an alkali reserve. The general rules governing the composition of the respective treatment
5 fluids apply here, for which exemplary indications are given below with reference to corresponding drilling muds. The additives may be water soluble, oil soluble and/or water-dispersible or oil-dispersible.

Conventional additives may be the following: fluid loss additives, soluble and/or insoluble substances which provide pseudoplasticity, alkali reserves, agents for
10 inhibiting the unwanted exchange of water between drilled formations – e.g. water-swellable clays and/or salt strata – and the drilling fluid which is based for example on water, wetting agents for better attachment of the emulsified oil phase to surfaces of solids, for the purpose of improving the lubricating effect, for example, but also for improving the oleophilic sealing of exposed rock formations or rock
15 faces, biocides, for example for inhibiting the bacterial infestation of O/W emulsions and the like. Merely by way of example mention may be made accordingly of finely disperse additives for increasing the density of the mud: in widespread use is barium sulphate (barytes), although calcium carbonate (calcite) and the mixed carbonate of calcium and magnesium (dolomite) are also in use.

20 Agents for building up pseudoplasticity, which at the same time also act as fluid loss additives: mention should be made here primarily of bentonite, including hydrophobicized bentonite. For saltwater muds, other, comparable clays, especially attapulgite and sepiolite, are of considerable importance in practice.

The use of organic polymer compounds of natural and/or synthetic origin may also
25 be accorded considerable significance in this context. They include, in particular, starch or chemically modified starches, cellulose derivatives such as carboxymethylcellulose, guar gum, xanthan gum or else purely synthetic, water-soluble and/or water-dispersible polymer compounds, especially those of the type of high molecular mass polyacrylamide compounds with or without anionic and/or cationic
30 modification. Diluents for regulating viscosity: the diluents, as they are known, may be organic or inorganic in nature. Examples of organic diluents are tannins

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and/or quebracho extract. Further examples thereof are lignite and lignite derivatives, especially lignosulfonates.

As indicated above, however, in one preferred embodiment of the invention the use of toxic components is specifically avoided here, reference here being primarily to
5 the corresponding salts with toxic heavy metals such as chromium and/or copper. An example of inorganic diluents are polyphosphate compounds. Additives which inhibit the unwanted exchange of water with, for example, clays: suitable here are the additives known from the prior art for oil- and water-based drilling muds. These additives include, in particular, halides and/or carbonates of the alkali metals
10 and/or alkaline earth metals, it being possible to accord particular importance to corresponding potassium salts in combination where appropriate with lime.

Alkali reserves: suitable here are organic and/or inorganic bases matched to the overall properties of the mud, especially corresponding basic salts and/or hydroxides of alkali metals and/or alkaline earth metals, and also organic bases. Particular
15 preference here is given to the use of lime (Ca(OH)_2) as alkali reserve. Typical levels of lime in the drilling mud are between 1 and 6 lb/bbl, the amounts which can be used depending critically on the nature and composition of the oil phase. The nature and amount of these basic components are preferably chosen and matched to one another such that in the case of esters susceptible to hydrolysis,
20 particularly unsaturated esters with carbon numbers from C16 to C24, excessive hydrolysis does not occur, since the resulting reaction products, especially the fatty acids, may adversely affect the stability of the emulsion drilling mud. It is preferred in these cases to provide an alkali reserve in the mud which corresponds at most to a concentration of 2 lb/bbl of the basic component, preferably lime, in the
25 mud under operation conditions.

In the field of organic bases a terminological distinction is to be made between water-soluble organic bases – for example, compounds of the diethanolamine type – and virtually water-insoluble bases of pronounced oleophilic character. The additional use of such oil-soluble bases is specifically part of the teaching of the pre-
30 sent invention. Oleophilic bases of this kind, which are distinguished in particular by at least one relatively long hydrocarbon radical having, for example, from 8 to

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36 carbon atoms, are in that case not, however, dissolved in the aqueous phase but rather in the oil phase. Here, multiple significance is accorded to these basic components. On the one hand, they may act directly as an alkali reserve. On the other, they give the dispersed oil droplets a certain positive state of charge and so lead to
5 increased interaction with negative surface charges such as are encountered in particular with hydrophilic clays that are capable of ion exchange. In accordance with the invention it is thereby possible to exert influence on the hydrolytic cleavage and the oleophilic sealing of water-reactive rock strata. The amount of the auxiliaries and additives employed in each case is fundamentally within customary ranges
10 and can therefore be taken from the relevant cited literature.

The use of the esters of group c) in a blend with component a) and/or b) means that it is possible to obtain oil phases which are of low relative toxicity towards the marine microbiont *Leptocheirus plumulosus*.

15 In addition, however, the addition of esters of the general formula $R-COO-R'$ in which R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical having from 3 to 10 carbon atoms markedly improves the lubricating properties of drilling muds comprising an aqueous phase and a non-aqueous oil
20 phase, emulsifiers and, where appropriate, further customary additives, such as weighting agents, fluid loss additives, viscosity regulators, wetting agents, salts, biocides, corrosion inhibitors and/or an alkali reserve. It is preferred to use between 5 and 15% by weight, in particular from 8 to 12% by weight, of these esters in the oil phase in order to obtain the desired lubricating effect.

25

Furthermore, it is possible by adding the esters of the general formula $R-COO-R'$ in which R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbons and R' denotes a saturated, linear or branched alkyl radical having from 3 to 10 carbon atoms to oil phases of customary drilling muds
30 to reduce the use of structuring agents, preferably products based on clays with or without chemical or physical modification, e.g., bentonites. For details, refer to the

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relevant literature, in this case, for example, the Manual of Drilling Fluid Technology, NL Baroid, 1979, Chapter on "Fundamental Characteristics of Drilling Fluids" and in particular the disclosure content of pages 5 to 8. Accordingly, considerable cost advantages arise as compared with prior art muds. The amounts in which
5 the inventively used esters are employed are between 15 and 100% by weight, preferably between 25 and 100% by weight and in particular from 50 to 100% by weight, based on the amount of the oil phase. By means of the oil phases of the invention it is possible to achieve marked reductions in the fraction of clay-based structuring agents. It is even possible to formulate clay-free muds. The esters are
10 preferably used in the context of the invention for emulsion drilling muds of the invert type, i.e. W/O.

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Examples

Set out below are examples of the low-toxicity drilling muds of the invention. Four different muds were produced, based on the following framework formula:

5

Oil phase 0.567 bbl

Water 0.148 bbl

Organophilic

bentonite 2.0 bbl Geltone, Baroid Company

10 Emulsifier 8.0 bbl (EZ-Mul NTE, Baroid Company)

Fluid loss

additive 8.00 bbl (Duratone HT, Baroid Company)

Lime 1.0 bbl

$\text{CaCl}_2 \cdot 2\text{H}_2\text{O}$ 18.0 bbl

15 Barytes 326.1 bbl

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Oil/water ratio: 80/20

Example 1

- 5 For Example 1 the oil phase used was a mixture (50:50 w/w) of 0.284 bbl of an IO mixture comprising C16/C18 IOs and a saturated monocarboxylic ester based on monocarboxylic acids having 20 to 22 carbon atoms and 2-ethylhexanol (OMC 586, Cognis Company). The F value was 0.87.

10 The tables below list the rheological characteristics in each case before and after ageing of the muds at 250°F for 16 h. The rheological data were in each case measured in accordance with API bulletin RP 13 B-2.

	Unaged	Aged	
Plastic viscosity (PV)	25	25	cP
Yield point (YP)	17	14	lb/100 ft ²
Gel strength 10 s/10 min.	7/8	6/6	lb/100 ft ²

Comparative Example 1

15

The mud of the Comparative Example contained in the oil phase only an IO mixture based on C16/C18 IOs. The F value, however, was 2.7.

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	Unaged	Aged	
Plastic viscosity (PV)	28	20	cP
Yield point (YP)	14	5	lb/100 ft ²
Gel strength 10 s/10 min.	6/7	4/6	lb/100 ft ²

It was found that the use of ester/paraffin mixtures allows low-toxicity drilling muds to be produced without any restriction on the service properties.

5 Example 2

For Example 2 a mud in analogy to Example 1 was used, but the content of the fluid loss additive was reduced to 4 lb. The F value was 0.87.

	Unaged	Aged	
Plastic viscosity (PV)	22	21	cP
Yield point (YP)	11	12	lb/100 ft ²
Gel strength 10 s/10 min.	5/6	5/7	lb/100 ft ²

10

Comparative Example 2:

Again, the Comparative Example used was a mud with exclusively IO in the oil phase.

15

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	Unaged	Aged	
Plastic viscosity (PV)	17	18	cP
Yield point (YP)	6	11	lb/100 ft ²
Gel strength 10 s/10 min.	3/4	3/4	lb/100 ft ²

Example 3

The following compilation shows the comparison of oil phases based on paraffin
5 with an oil phase based on a 1:1 paraffin/ester mixture (Ester: OMC586). The paraffin was Puredrill IA-35 from the Petro Canda Company. The remaining constituents of the mud were in accordance with the outline formula given above.

Examples after ageing (16h, 250°F), oil/water: 80/20:

10

	Paraffin	Paraffin Ester 1:1	Paraffin	Paraffin Ester 1:1	Paraffin	Paraffin Ester 1:1	Paraffin	Paraffin Ester 1:1
Geltone lb/bbl	0	0	0.5	0.5	1	1	2	2
PV	20	20	18	20	20	22	22	25
YP	2	10	3	14	3	11	3	12

Examples (before ageing)

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	Para-ffin	Paraffin Ester 1:1	Para- ffin	Paraffin Ester 1:1	Para- ffin	Paraffin Ester 1:1
Geltone lb/bbl	0	0	1	1	2	2
PV	18	23	19	22	23	27
YP	2	15	4	17	4	17

As is evident from the above results, it is possible to formulate systems based on paraffin/ester mixtures which have a greatly reduced Geltone content. Attempts to achieve such effects using mixtures of different aromatics-free/low-aromatics hydrocarbons were unsuccessful.

Another important criterion is the base viscosity of oil phases. Here, measurement is carried out by the Ubbelohde method at 20°C using the capillary factors $c = 0.009987$, $c = 0.009933$, $c = 0.029$. The kinematic viscosity is given by the formula $v = \Delta t \times c$. Ester based in each case on 2-ethylhexanol.

Examples:

$C_{16/18}$ IO + C_{20-22} esters	1:1	6.1 mm ² /s
Branched paraffin + C_{15-17} esters	1:1	4.9 mm ² /s
Branched paraffin + C_{20-22} esters	1:1	7.2 mm ² /s
Branched paraffin + C_{15-17} ester + C_{24-26} ester	1:1:0.5	6.1 mm ² /s
Branched paraffin + C_{24-26} + C_{24-26} esters	1:1	9.3 mm ² /s

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Claims

1. Borehole treatment composition comprising an aqueous phase and a non-
5 aqueous oil phase, emulsifiers and, where appropriate, further customary additives, such as weighting agents, fluid loss additives, viscosity regulators, wetting agents, salts, biocides, corrosion inhibitors and/or an alkali reserve, the non-aqueous phase being selected in whole or in part from the group consisting of
 - 10 a) paraffins having from 5 to 22 carbon atoms and/or
 - b) internal olefins having from 12 to 30 carbon atoms in the molecule
in each case in the form of a blend with
 - c) carboxylic esters of the general formula $R-COO-R'$, where R stands for a linear or branched, saturated or un-
15 saturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical having from 3 to 22 carbon atomscharacterized in that the ratio of the toxicity of internal olefins of chain length C16/C18 (standard IO) to the toxicity of the constituents of the non-
20 aqueous phase, in each case measured by the *Leptocheirus plumulosus* acute, static 96 hour/10 day sediment toxicity test (in accordance with ASTM E 1367 – 92 & EPA/600/R-94/025, Section 11), is less than 1.
2. Borehole treatment composition according to Claim 1, characterized in that
25 it is in water-in-oil (W/O) emulsion form.
3. Borehole treatment composition according to Claims 1 and 2, characterized in that it is formulated as a drilling mud.

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4. Borehole treatment composition according to Claims 1 to 3, characterized in that the weight ratio between the aqueous phase and the oil phase is from 50:50 to 1:99, preferably from 30:70 to 20:80 and in particular 10:90.
- 5
5. Borehole treatment composition according to Claims 1 to 4, characterized in that at least 50% by weight, preferably at least 80% by weight and in particular at least 90% by weight of the oil phase is composed of compounds a) and/or b) and c).
- 10
6. Borehole treatment composition according to one of Claims 1 to 5, characterized in that component a) is selected from the group consisting of linear and branched paraffins having from 10 to 21 carbon atoms, branched paraffins being particularly preferred.
- 15
7. Borehole treatment composition according to one of Claims 1 to 6, characterized in that component b) is selected from the group consisting of internal olefins having from 12 to 30 carbon atoms, preferably from 14 to 24 and in particular up to 20 carbon atoms.
- 20
8. Borehole treatment composition according to Claims 1 to 7, characterized in that component c) is selected from esters of the formula $R-COO-R'$ in which R stands for saturated or unsaturated linear alkyl radicals having from 15 to 23 carbon atoms and R' denotes a linear or branched saturated alkyl radical having from 6 to 22 carbon atoms.
- 25
9. Borehole treatment composition according to Claims 1 to 8, characterized in that in addition to the esters according to Claim 7 there is not more than

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15% by weight (based on the oil phase) of esters with radicals R which stand for alkyl radicals having more than 23 carbon atoms.

- 5 10. Borehole treatment composition according to Claims 1 to 9, characterized in that 100% by weight of the non-aqueous oil phase is composed of the compounds a) and/or b) and c).
- 10 11. Borehole treatment composition according to Claims 1 to 10, characterized in that at least 50% by weight, preferably at least 80% by weight and in particular 100% by weight of the non-aqueous oil phase comprises blends of compounds b) and c).
- 15 12. Borehole treatment composition according to Claims 1 to 11, characterized in that in addition to the compounds a) to c) there are further, environmentally compatible, water-insoluble components present.
- 20 13. Borehole treatment composition according to Claims 1 to 12, characterized in that as a further component use is made of esters of C1-C5 monocarboxylic acids with mono- and/or polyfunctional alcohols, the alcohols having at least 6, preferably at least 8, and the polyhydric alcohols from 2 to 6, carbon atoms per molecule.
- 25 14. Borehole treatment composition according to Claims 1 to 13, characterized in that further components present in the non-aqueous oil phase include mixtures of secondary esters selected from the group consisting of propyl carboxylate, butyl carboxylate, pentyl carboxylate, hexyl carboxylate, heptyl carboxylate, octyl carboxylate, nonyl carboxylate, decyl carboxylate, undecyl carboxylate, dodecyl carboxylate, tridecyl carboxylate, tetradecyl carboxylate, pentadecyl carboxylate, hexadecyl carboxylate, heptadecyl

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carboxylate, octadecyl carboxylate, nonadecyl carboxylate, eicosyl carboxylate, uneicosyl carboxylate, docicosyl carboxylate and isomers thereof, the secondary esters each having a carboxylate radical of 1 to 5 carbon atoms.

5

15. Borehole treatment composition according to Claims 1 to 14, characterized in that the non-aqueous oil phase has a pour point of below 0°C, preferably below -5°C.

10 16. Borehole treatment composition according to Claims 1 to 15, which as an oil-based drilling mud of the W/O type has a plastic viscosity (PV) in the range from 10 to 70 mPas and a yield point (YP) from 5 to 60 lb/100 ft², measured in each case at 50°C, characterized in that the non-aqueous oil phase has a Brookfield viscosity at 0°C of not more than 50 mPas.

15

17. Borehole treatment composition according to Claims 1 to 16, characterized in that as an oil-based drilling mud of the W/O type it has a plastic viscosity (PV) in the range from 10 to 60 mPas and a yield point (YP) from 5 to 40 lb/100 ft², measured in each case at 50°C.

20

18. Borehole treatment composition according to Claims 1 to 17, characterized in that the oil phase has an Ubbelohde viscosity at 20°C of not more than 12 mm²/s.

25 19. Borehole treatment composition according to Claims 1 to 18, characterized in that the aqueous phase has a pH in the range from 7.5 to 12, preferably from 7.5 to 11 and in particular from 8 to 10.

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20. Borehole treatment composition according to Claims 1 to 19, characterized in that the non-aqueous oil phase comprises blends of components a) or b) and c) in a weight ratio of from 10:1 to 1:1, preferably from 5:1 to 1:1 and in particular from 3:1 to 1:1.
- 5
21. Borehole treatment composition according to Claims 1 to 20, characterized in that it comprises non-aqueous components b) whose relative toxicity in relation to standard IOs of chain length C16/C18 is greater than 1, it being necessary for compounds according to c) to be present in the non-aqueous oil phase.
- 10
22. Use of blends of a) linear or branched paraffins having from 10 to 22 carbon atoms and/or b) internal olefins having from 12 to 30 carbon atoms per molecule with c) carboxylic esters of the general formula $R-COO-R'$ in which R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical having from 3 to 22 carbon atoms for producing invert drilling muds of low toxicity.
- 15
23. Use of esters of the formula $R-COO-R'$ in which R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical having from 3 to 22 carbon atoms as a mixture constituent in invert drilling muds which comprise paraffins and/or internal olefins as constituents of the oil phase for reducing the toxicity of the oil phase of the invert drilling muds, measured by the *Leptocheirus plumulosus* acute, static 96 hour/10 day sediment toxicity test (in accordance with ASTM E 1367 - 92 & EPA/600/R-94/025, Section 11).
- 20
- 25

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24. Drilling mud comprising an aqueous phase and a non-aqueous oil phase, emulsifiers and, where appropriate, further customary additives, such as weighting agents, fluid loss additives, viscosity regulators, wetting agents, salts, biocides, corrosion inhibitors and/or an alkali reserve, more than 50%
5 by weight of the non-aqueous phase being selected from the group consisting of esters of the general formula $R-COO-R'$ in which R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical having from 3 to 10 carbon atoms, the drilling mud having a relative toxicity,
10 i.e. the ratio of the toxicity of internal olefins of chain length C16/C18 (standard IO) to the toxicity of the constituents of the non-aqueous phase, in each case measured by the *Leptocheirus plumulosus* acute, static 96 hour/10 day sediment toxicity test (in accordance with ASTM E 1367 – 92 & EPA/600/R-94/025, Section 11), of less than 1.
- 15
25. Use of esters of the general formula $R-COO-R'$ in which R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical having from 3 to 10 carbon atoms as an additive to drilling muds comprising
20 an aqueous phase and a non-aqueous oil phase, emulsifiers and, where appropriate, further customary additives, such as weighting agents, fluid loss additives, viscosity regulators, wetting agents, salts, biocides, corrosion inhibitors and/or an alkali reserve, for improving the lubricating properties of the drilling muds.
- 25
26. Use of esters of the general formula $R-COO-R'$ in which R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical having from 3 to 10 carbon atoms as an additive to drilling muds comprising
30 an aqueous phase and a non-aqueous oil phase, emulsifiers and, where appropriate, further customary additives, such as weighting agents, fluid

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loss additives, viscosity regulators, wetting agents, salts, biocides, corrosion inhibitors and/or an alkali reserve, for reducing the fraction of structuring agents based on clays with or without chemical or physical modification.

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Abstract

A description is given of borehole treatment compositions comprising an aqueous phase and a non-aqueous oil phase, emulsifiers and, where appropriate, further
5 customary additives, such as weighting agents, fluid loss additives, viscosity regulators, wetting agents, salts, biocides, corrosion inhibitors and/or an alkali reserve, the non-aqueous phase being selected in whole or in part from the group consisting of

- a) paraffins having from 5 to 22 carbon atoms and/or
- 10 b) internal olefins having from 12 to 30 carbon atoms in the molecule
in each case in the form of a blend with
- c) carboxylic esters of the general formula $R-COO-R'$, where R stands for a linear or branched, saturated or unsaturated alkyl radical having from 15 to 25 carbon atoms and R' denotes a saturated, linear or branched alkyl radical
15 having from 3 to 22 carbon atoms

characterized in that the ratio of the toxicity of internal olefins of chain length C16/C18 (standard IO) to the toxicity of the constituents of the non-aqueous phase, in each case measured by the *Leptocheirus plumulosus* acute, static 96 hour/10 day sediment toxicity test (in accordance with ASTM E 1367 – 92 &
20 EPA/600/R-94/025, Section 11), is less than 1.